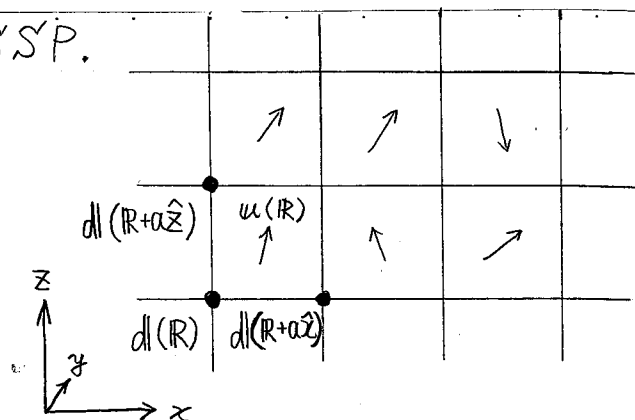


On acoustic displacements

$d = \begin{pmatrix} d_x \\ d_y \\ d_z \end{pmatrix}$, Let's use the notations of strain same as chapter 3 of Kittel's ISSP.

$$d_\alpha(\mathbf{R}) = \frac{1}{N} \sum_{\mathbf{k}} \tilde{d}_\alpha(\mathbf{k}) e^{i\mathbf{k} \cdot \mathbf{R}}$$

$$\tilde{d}_\alpha(\mathbf{k}) = \sum_{\mathbf{R}} d_\alpha(\mathbf{R}) e^{-i\mathbf{k} \cdot \mathbf{R}}$$



$$\epsilon_{xx}(\mathbf{R}) = \frac{1}{a} [d_x(\mathbf{R} + a\hat{x}) - d_x(\mathbf{R})]$$

$$= \frac{1}{a} \frac{\partial d_x(\mathbf{R})}{\partial x} a = \frac{\partial d_x(\mathbf{R})}{\partial x}$$

$$= \frac{1}{N} \sum_{\mathbf{k}} \tilde{d}_x(\mathbf{k}) i k_x e^{i\mathbf{k} \cdot \mathbf{R}}$$

Fourier coefficients \longrightarrow Check it!

$$\tilde{\epsilon}_{xx}(\mathbf{k}) = \sum_{\mathbf{R}} \epsilon_{xx}(\mathbf{R}) e^{-i\mathbf{k} \cdot \mathbf{R}}$$

$$= \sum_{\mathbf{R}} \left(\frac{1}{N} \sum_{\mathbf{k}'} \tilde{d}_x(\mathbf{k}') i k'_x e^{i\mathbf{k}' \cdot \mathbf{R}} \right) e^{-i\mathbf{k} \cdot \mathbf{R}}$$

$$= \frac{1}{N} \sum_{\mathbf{R}} \sum_{\mathbf{k}'} \tilde{d}_x(\mathbf{k}') i k'_x e^{i(\mathbf{k}' - \mathbf{k}) \cdot \mathbf{R}}$$

$$= \frac{1}{N} \sum_{\mathbf{R}} \tilde{d}_x(\mathbf{k}) i k_x = \tilde{d}_x(\mathbf{k}) i k_x \quad \text{--- } \star 1$$

\longrightarrow Of course!

Similarly,

$$\epsilon_{xy}(\mathbf{R}) = \frac{1}{N} \sum_{\mathbf{k}} \tilde{d}_x(\mathbf{k}) i k_y e^{i\mathbf{k} \cdot \mathbf{R}}, \quad \tilde{\epsilon}_{xy}(\mathbf{k}) = \tilde{d}_x(\mathbf{k}) i k_y$$

$$\epsilon_{yx}(\mathbf{R}) = \frac{1}{N} \sum_{\mathbf{k}} \tilde{d}_y(\mathbf{k}) i k_x e^{i\mathbf{k} \cdot \mathbf{R}}, \quad \tilde{\epsilon}_{yx}(\mathbf{k}) = \tilde{d}_y(\mathbf{k}) i k_x$$

BTW,

$$\eta_i(\mathbf{R}) = \epsilon_{xy}(\mathbf{R}) + \epsilon_{yx}(\mathbf{R})$$

$$\tilde{\eta}_i(\mathbf{k}) =$$

$$= \frac{1}{N} \sum_{\mathbf{k}} i [d_x(\mathbf{k}) k_y + d_y(\mathbf{k}) k_x] e^{i\mathbf{k} \cdot \mathbf{R}}$$

$$\tilde{\epsilon}_{xy}(\mathbf{k}) = i [d_x(\mathbf{k}) k_y + d_y(\mathbf{k}) k_x]$$

--- $\star 2$

$$V^{\text{coup, inho}}(\mathbf{R})$$

$$= V^{\text{coup, inho}}(\eta_1(\mathbf{R}), \dots, \eta_6(\mathbf{R}); \gamma_1(\mathbf{R}), \dots, \gamma_6(\mathbf{R}))$$

$$= \frac{1}{2} \begin{pmatrix} \eta_1(\mathbf{R}) & \dots & \eta_6(\mathbf{R}) \end{pmatrix} \begin{pmatrix} \gamma_1(\mathbf{R}) \\ \gamma_2(\mathbf{R}) \\ \vdots \\ \gamma_6(\mathbf{R}) \end{pmatrix}$$

\leftrightarrow
Eq. (21) of
Nishimatsu 2008

$$\sum_{\mathbf{R}} V^{\text{coup, inho}}(\mathbf{R})$$

$$= \frac{1}{2} \sum_{\mathbf{R}} \frac{1}{N} \sum_{\mathbf{k}} \frac{1}{N} \sum_{\mathbf{k}'} \begin{pmatrix} d_x(\mathbf{k}') i k_x' \\ d_y(\mathbf{k}') i k_y' \\ d_z(\mathbf{k}') i k_z' \\ d_y(\mathbf{k}) i k_z' + \tilde{d}_z(\mathbf{k}) i k_y' \\ d_z(\mathbf{k}) i k_x' + \tilde{d}_x(\mathbf{k}) i k_z' \\ d_x(\mathbf{k}) i k_y' + \tilde{d}_y(\mathbf{k}) i k_x' \end{pmatrix} \begin{pmatrix} \tilde{\gamma}_1(\mathbf{k}) \\ \vdots \\ \tilde{\gamma}_6(\mathbf{k}) \end{pmatrix} e^{i(\mathbf{k}+\mathbf{k}')\cdot\mathbf{R}}$$

$\mathbf{k} = -\mathbf{k}'$
のときのみ
値をもつ
から、

$$= \frac{1}{2N^2} \sum_{\mathbf{R}} \sum_{\mathbf{k}} \begin{pmatrix} \tilde{d}_x(-\mathbf{k}) (-i k_x) \\ \vdots \\ \tilde{d}_x(-\mathbf{k}) (-i k_y) + \tilde{d}_y(-\mathbf{k}) (-i k_z) \end{pmatrix} \begin{pmatrix} \tilde{\gamma}_1(\mathbf{k}) \\ \vdots \\ \tilde{\gamma}_6(\mathbf{k}) \end{pmatrix}$$

$$= \frac{1}{2N} \sum_{\mathbf{k}} (-i) \begin{pmatrix} d_x^*(\mathbf{k}) k_x \\ \vdots \\ \tilde{d}_x^*(\mathbf{k}) k_y + \tilde{d}_y^*(\mathbf{k}) k_x \end{pmatrix} \begin{pmatrix} \tilde{\gamma}_1(\mathbf{k}) \\ \vdots \\ \tilde{\gamma}_6(\mathbf{k}) \end{pmatrix} \quad (22)$$

$$x^*(\mathbf{k}) C y(\mathbf{k}) + x^*(-\mathbf{k}) C y(-\mathbf{k})$$

$$= x^*(\mathbf{k}) C y(\mathbf{k}) + x(\mathbf{k}) C y^*(\mathbf{k})$$

$$= x^*(\mathbf{k}) C y(\mathbf{k}) + [x^*(\mathbf{k}) C y(\mathbf{k})]^*$$

$$= 2 \text{Re}[x^*(\mathbf{k}) C y(\mathbf{k})]$$

2 π^0 -ジ前にはスト
の様子を貼付けた。
energy-module.F (rev1617) の下の
ほうで、 $\{\mathbf{k}\}$ のうち半分で summation
... ..

2012-12-12

$$K \swarrow$$
$$\begin{pmatrix} \tilde{d}_x & \tilde{d}_y & \tilde{d}_z \end{pmatrix} \begin{pmatrix} k_x & 0 & 0 & 0 & k_z & k_y \\ 0 & k_y & 0 & k_z & 0 & k_x \\ 0 & 0 & k_z & k_y & k_x & 0 \end{pmatrix}$$
$$= (\tilde{d}_x k_x \quad \tilde{d}_y k_y \quad \tilde{d}_z k_z \quad \tilde{d}_y k_z + \tilde{d}_z k_y \quad \tilde{d}_z k_x + \tilde{d}_x k_z \quad \tilde{d}_x k_y + \tilde{d}_y k_x)$$

$$\begin{pmatrix} k_x & 0 & 0 & 0 & k_z & k_y \\ 0 & k_y & 0 & k_z & 0 & k_x \\ 0 & 0 & k_z & k_y & k_x & 0 \end{pmatrix} \begin{pmatrix} B_{1xx} & B_{1yy} & B_{1yz} & 0 \\ B_{1yz} & B_{xx} & B_{yz} & 0 \\ B_{1yz} & B_{1yz} & B_{xx} & 0 \\ 0 & 0 & 2B_{4yz} & 0 \\ 0 & 2B_{4yz} & 0 & 0 \\ 0 & 0 & 2B_{4yz} & 0 \end{pmatrix}$$

$$= \begin{pmatrix} k_x B_{1xx} & k_x B_{1yy} & k_x B_{1zz} & 0 & 2k_z B_{4yz} & 2k_y B_{4yz} \\ k_y B_{1xx} & k_y B_{1yy} & k_y B_{1zz} & 2k_z B_{4yz} & 0 & 2k_x B_{4yz} \\ k_z B_{1xx} & k_z B_{1yy} & k_z B_{1zz} & 2k_y B_{4yz} & 2k_x B_{4yz} & 0 \end{pmatrix}$$

$$\text{Eg. (16)} \quad (x_1 \dots x_6) \begin{pmatrix} B_{11} & B_{12} & B_{12} & 0 & 0 & 0 \\ B_{12} & B_{11} & B_{12} & 0 & 0 & 0 \\ B_{12} & B_{12} & B_{11} & 0 & 0 & 0 \\ 0 & 0 & 0 & B_{44} & 0 & 0 \\ 0 & 0 & 0 & 0 & B_{44} & 0 \\ 0 & 0 & 0 & 0 & 0 & B_{44} \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \\ x_5 \\ x_6 \end{pmatrix}$$

Eg. (17), (18), (19)

$$\Phi^{\text{elas, inh}}(\mathbb{K}) = \frac{1}{N} \mathbb{K} \mathbb{B}^T \mathbb{K}$$

$$E_{\text{g.}} (24), (25) \Rightarrow V^{\text{coup}, \{ \text{homo} \}}_{\text{in ho}} = -2 V^{\text{elas}, \{ \text{homo} \}}_{\text{in ho}}$$

B. Molecular dynamics

MD simulations with the effective Hamiltonian of Eq. (4) are performed in the canonical ensemble using the Nosé-Poincaré thermostat.¹⁶ This symplectic thermostat is so efficient that we can set the time step to $\Delta t = 2$ fs. In our present simulations, we thermalize the system for 40,000 time steps, after which we average the properties for 10,000 time steps.

In Fig. 1 we roughly illustrate how to calculate the forces exerted on $u_\alpha(\mathbf{R})$ with $\tilde{\Phi}_{\alpha\beta}^{\text{quad}}(\mathbf{k})$ in Eq. (13) and how the time evolution is simulated. First, $u_\alpha(\mathbf{R})$ is FFTed to $\tilde{u}_\alpha(\mathbf{k})$, the force $\tilde{F}_\alpha(\mathbf{k}) = -\sum_\beta \tilde{\Phi}_{\alpha\beta}^{\text{quad}}(\mathbf{k}) \tilde{u}_\beta(\mathbf{k})$ is calculated in reciprocal space, and then the force in real space is obtained by the inverse FFT (IFFT) of $\tilde{F}_\alpha(\mathbf{k})$. In practice, updates of $u_\alpha(\mathbf{R})$ and $\dot{u}_\alpha(\mathbf{R}) = \frac{\partial}{\partial t} u_\alpha(\mathbf{R})$ are processed in the manner of the Nosé-Poincaré thermostat.

The homogeneous strain components η_1, \dots, η_6 are determined by solving

$$\frac{\partial}{\partial \eta_i} [V^{\text{elas,homo}}(\eta_1, \dots, \eta_6) + V^{\text{coup,homo}}(\{\mathbf{u}\}, \eta_1, \dots, \eta_6)] = 0 \quad (24)$$

at each time step according to $\{\mathbf{u}\}$ so that η_1, \dots, η_6 minimize $V^{\text{elas,homo}}(\eta_1, \dots, \eta_6) + V^{\text{coup,homo}}(\{\mathbf{u}\}, \eta_1, \dots, \eta_6)$. While the local acoustic displacement $w_\alpha(\mathbf{R})$ could be treated as dynamical variables using the effective mass M_{acoustic}^* , we have instead chosen to integrate out these variables in a manner similar to the treatment of the homogeneous strain. That is, $w_\alpha(\mathbf{R})$ is determined so that $V^{\text{elas,inho}}(\{\mathbf{w}\}) + V^{\text{coup,inho}}(\{\mathbf{u}\}, \{\mathbf{w}\})$ becomes minimum at each time step according to $u_\alpha(\mathbf{R})$. Technically, the minimization is performed by solving the linear set of equations

$$\tilde{\Phi}^{\text{elas,inho}}(\mathbf{k}) \tilde{\mathbf{w}}(\mathbf{k}) + \tilde{\mathbf{B}}(\mathbf{k}) \tilde{\mathbf{y}}(\mathbf{k}) = 0 \quad (25)$$

for each \mathbf{k} in reciprocal space.

The homogeneous elastic energy $V^{\text{elas,homo}}(\eta_1, \dots, \eta_6)$ is

$$V^{\text{elas,homo}}(\eta_1, \dots, \eta_6) = \frac{N}{2} B_{11} (\eta_1^2 + \eta_2^2 + \eta_3^2) + N B_{12} (\eta_2 \eta_3 + \eta_3 \eta_1 + \eta_1 \eta_2) + \frac{N}{2} B_{44} (\eta_4^2 + \eta_5^2 + \eta_6^2), \quad (16)$$

where B_{11} , B_{12} , and B_{44} are the elastic constants expressed in energy unit ($B_{11} = a_0^3 C_{11}$, $B_{12} = a_0^3 C_{12}$, and $B_{44} = a_0^3 C_{44}$).

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The inhomogeneous elastic energy $V^{\text{elas,inho}}(\{\mathbf{w}\})$ is also calculated in reciprocal space as

$$V^{\text{elas,inho}}(\{\mathbf{w}\}) = \frac{1}{2} \sum_{\mathbf{k}} \sum_{\alpha, \beta} \tilde{w}_\alpha^*(\mathbf{k}) \tilde{\Phi}_{\alpha\beta}^{\text{elas,inho}}(\mathbf{k}) \tilde{w}_\beta(\mathbf{k}). \quad (17)$$

For the force constant matrix $\tilde{\Phi}_{\alpha\beta}^{\text{elas,inho}}(\mathbf{k})$, we employed the long-wavelength approximation. For instance, the diagonal part is

$$\tilde{\Phi}_{\alpha\beta}^{\text{elas,inho}}(\mathbf{k}) = \frac{1}{N} [k_x^2 B_{11} + k_y^2 B_{44} + k_z^2 B_{44}], \quad (18)$$

and the off-diagonal part is

$$\tilde{\Phi}_{\alpha\beta}^{\text{elas,inho}}(\mathbf{k}) = \frac{1}{N} [k_x k_y B_{12} + k_x k_y B_{44}]. \quad (19)$$

The coupling between $\{\mathbf{u}\}$ and homogeneous strain is the same as that given in Ref. 9, i.e.,

$$V^{\text{coup,homo}}(\{\mathbf{u}\}, \eta_1, \dots, \eta_6) = \frac{1}{2} \sum_{\mathbf{R}} \sum_{i=1}^6 \sum_{j=1}^6 \eta_i C_{ij} y_j(\mathbf{R}). \quad (20)$$

Here, $y_1(\mathbf{R}) = u_x^2(\mathbf{R})$, $y_2(\mathbf{R}) = u_y^2(\mathbf{R})$, $y_3(\mathbf{R}) = u_z^2(\mathbf{R})$, $y_4(\mathbf{R}) = u_y(\mathbf{R}) u_z(\mathbf{R})$, $y_5(\mathbf{R}) = u_z(\mathbf{R}) u_x(\mathbf{R})$, and $y_6(\mathbf{R}) = u_x(\mathbf{R}) u_y(\mathbf{R})$,

$$\mathbf{C} = \begin{pmatrix} B_{1xx} & B_{1yy} & B_{1yy} & 0 & 0 & 0 \\ B_{1yy} & B_{1xx} & B_{1yy} & 0 & 0 & 0 \\ B_{1yy} & B_{1yy} & B_{1xx} & 0 & 0 & 0 \\ 0 & 0 & 0 & 2B_{4yz} & 0 & 0 \\ 0 & 0 & 0 & 0 & 2B_{4yz} & 0 \\ 0 & 0 & 0 & 0 & 0 & 2B_{4yz} \end{pmatrix}, \quad (21)$$

and B_{1xx} , B_{1yy} , and B_{4yz} are the coupling coefficients defined in Ref. 9.

The coupling between $\{\mathbf{u}\}$ and inhomogeneous strain is also calculated in reciprocal space as

$$V^{\text{coup,inho}}(\{\mathbf{u}\}, \{\mathbf{w}\}) = \frac{1}{2} \sum_{\mathbf{k}} \sum_{\alpha} \sum_{i=1}^6 \tilde{w}_\alpha^*(\mathbf{k}) \tilde{B}_{\alpha i}(\mathbf{k}) \tilde{y}_i(\mathbf{k}), \quad (22)$$

where $\tilde{w}_\alpha(\mathbf{k})$ and $\tilde{y}_i(\mathbf{k})$ are the Fourier transforms of $w_\alpha(\mathbf{R})$ and $y_i(\mathbf{R})$, respectively. For the 3×6 coupling matrix $\tilde{\mathbf{B}}(\mathbf{k})$, we again employed the long-wavelength approximation

$$\tilde{\mathbf{B}}(\mathbf{k}) = \frac{1}{N} \begin{pmatrix} k_x B_{1xx} & k_x B_{1yy} & k_x B_{1yy} & 0 & 2k_z B_{4yz} & 2k_y B_{4yz} \\ k_y B_{1yy} & k_y B_{1xx} & k_y B_{1yy} & 2k_z B_{4yz} & 0 & 2k_x B_{4yz} \\ k_z B_{1yy} & k_z B_{1yy} & k_z B_{1xx} & 2k_y B_{4yz} & 2k_x B_{4yz} & 0 \end{pmatrix}. \quad (23)$$

$\frac{1}{N}$ is O.K.
See Eq. (14)

In the present MD simulations of BaTiO₃, the parameters from Refs. 10 and 11, which are determined by first-

principles calculations, are employed. As mentioned in Refs. 10 and 11, this parameter set leads to an underestimation of the T_c .

2012-12-18

On optimize-info-strain.F and energy-module.F,

if we use $d_\alpha(k)$,

$$V^{\text{elas, inho}}(\{d(k)\}) = \frac{1}{2} \sum_k \tilde{d}^\dagger(k) \tilde{\Phi}(k) d(k)$$

$$V^{\text{coup, inho}}(\{d(k)\}, \{y(k)\}) = (-i) \sum_k \tilde{d}^\dagger(k) \left(\frac{1}{2} \tilde{B}(k) \right) \tilde{y}(k).$$

To minimize sum of them, $V^{\text{elas, inho}}(\{d(k)\}) + V^{\text{coup, inho}}(\{d(k)\}, \{y(k)\})$,

$$\tilde{\Phi}(k) d(k) - i \left(\frac{1}{2} \tilde{B}(k) \right) \tilde{y}(k) = 0. \quad (25)'$$

Now, let's define $\tilde{w}_\alpha(k)$ with

$$\tilde{d}_\alpha(k) = \left[-i \tilde{w}_\alpha(k) \right],$$

$$\tilde{d}_\alpha^*(k) = i \tilde{w}_\alpha^*(k).$$

In other words

$$d_\alpha(R) = \frac{1}{N} \sum_k \left[-i \tilde{w}_\alpha(k) \right] e^{ik \cdot R}$$

and

$$[-i \tilde{w}(k)] = \sum_R d_\alpha(R) e^{-ik \cdot R}.$$

Using this $\tilde{w}_\alpha(k)$, Eq. *1 and *2 become

$$\tilde{E}_{xx}(k) = \tilde{E}_{xx}(k) = \tilde{\eta}_1(k) = \tilde{w}_x(k) k_x$$

and

$$\tilde{E}_{xy}(k) = \tilde{\eta}_6(k)$$

$$= \tilde{E}_{xy}(k) + \tilde{E}_{yx}(k) = \tilde{w}_x(k) k_y + \tilde{w}_y(k) k_x.$$

Eq. (22)' becomes Eq. (22) in [Nishimatsu 2008].

And, Eq. (25)' becomes that of Eq. (25).

Up until now (and from now on), optimize-info-strain.F and energy-module.F are implemented with this $\tilde{w}_\alpha(k)$, $\text{acouK}(ix, iy, iz, \alpha)$.